



01092901

Phone (303) 522-8387

PICK TESTERS

Box 341
Sterling, CO 80751

RECEIVED

Contractor Ashby Drilling
Rig No. 1
Spot SW/NE
Sec 28
Twp. 2 N
Rng. 53 W
Field First Born
County Washington
State Colorado
Elevation 4648' KB
Formation D Sand

Surface Choke 1"
Bottom Choke 3/4"
Hole Size 7 7/8"
Core Hole Size --
DP Size & Wt. 4 1/2" 16.60
Wt. Pipe --
I.D. of DC 2 1/4"
Length of DC 566'
Total Depth 4969'
Type Test Straddle
Interval 4778'- 4796'

Mud Type Polymer/Gel
Weight 9.4
Viscosity 62
Water Loss
Filter Cake
Resistivity 2.8 @ 60 °F
2,271 Ppm. NaCl
B.H.T. 146 °F
Co. Rep. R. Eggelston
Tester A. Peterson
David Pickering

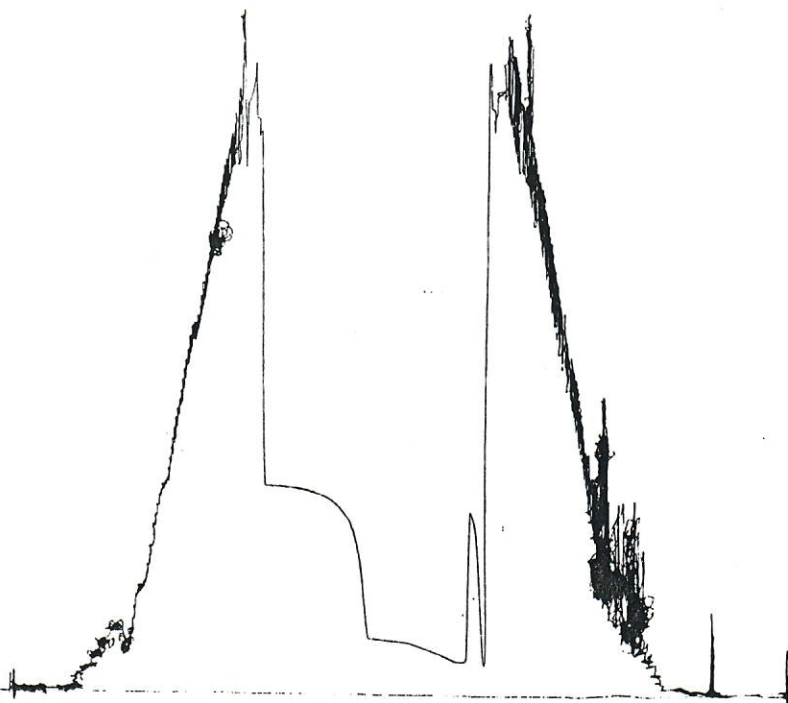
SEP 11 1997
COGCCCOMPANY
LEASE NAME & NO.
INTERVAL TESTEDPETERSON ENERGY/NEWPORT EXPL.
FASSLER #32-28
4778'- 4796'COUNTY
STATE
FORMATION
WASHINGTON
COLORADO
D SANDDATE
TICKET #
TEST #
10-26-1997
1587
1

REPORTED CORRECTED

Opened Tool @ 15:44 hrs.
Flow No. 1 1 1 min.
Shut-in No. 1 10 8 min.
Flow No. 2 60 57 min.
Shut-in No. 2 60 62 min.
Flow No. 3 min.
Shut-in No. 3 min.

Recorder Type Mechanical
No. 13338 Cap. 4950 psi
Depth 4804 feet
Inside x Clock
Outside Range 12 hrs.

Initial Hydrostatic A 2371
Final Hydrostatic K 2317
Initial Flow B 123
Final Initial Flow C 126
Initial Shut-in D 726
Second Initial Flow E 134
Second Final Flow F 223
Second Shut-in G 825
Third Initial Flow H
Third Final Flow I
Third Shut-in J



Pipe Recovery

536' Total fluid = 2.63 bbl., consisting of:
200' Slightly gas cut, oil cut mud = 0.98 bbl.
336' Slightly oil & gas cut water = 1.65 bbl.

Bottom: 2.2 @ 66 Deg F/1.05 @ Res Temp/2,674 ppm NaCl., 1,626 ppm Cl.

1st Flow: Tool opened with a slight blow, increased to 3" in 1 minute.

2nd Flow: Tool opened with a 1/4" blow, increased to a good blow off bottom of bucket in 8 minutes with 0.8 psi and continued to increase to 5.0 psi in 60 minutes. Gas to surface during the final shut-in period.

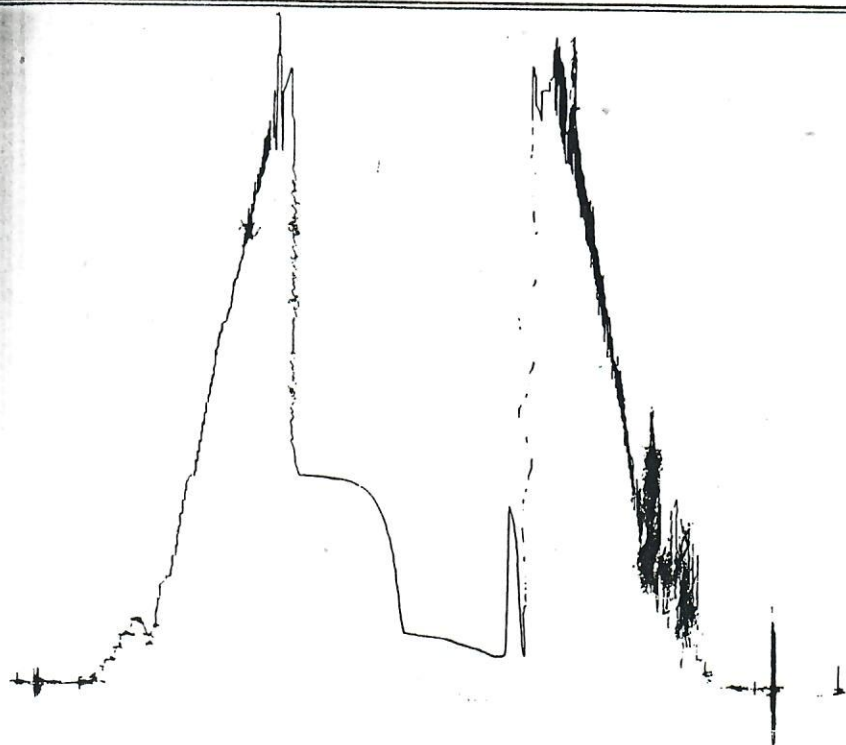
Peterson Energy/Newport Exploration
 Fassler #32-28
 DST #1

RECEIVED

SEP 11 01

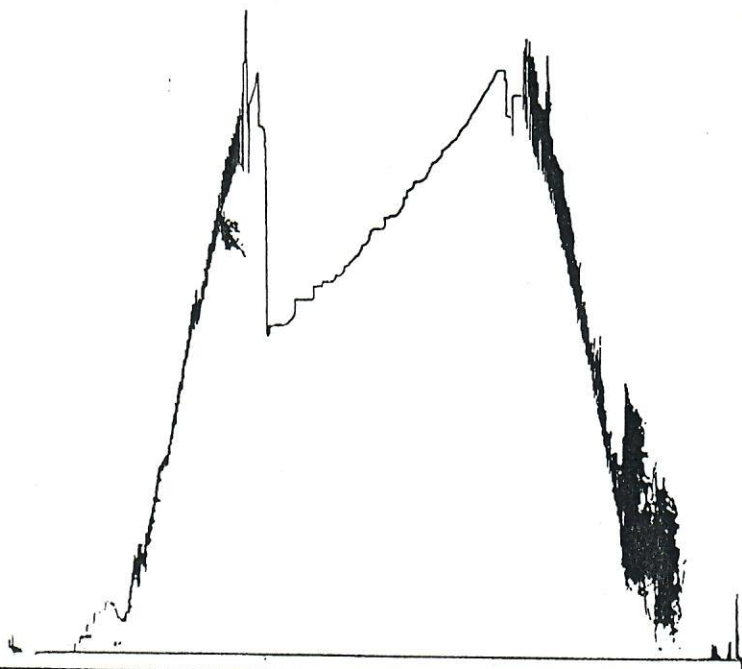
COGCC

10-26-1997



Recorder Type	Mechanical	
No. 13617	Cap. 4550	psi
Depth	4786	feet
Inside x	Clock	
Outside	Range 12	hrs.

Initial Hydrostatic	A	2369
Final Hydrostatic	K	2321
Initial Flow	B	123
Final Initial Flow	C	123
Initial Shut-In	D	700
Second Initial Flow	E	125
Second Final Flow	F	202
Second Shut-In	G	818
Third Initial Flow	H	
Third Final Flow	I	
Third Shut-In	J	



Recorder Type	Mechanical	
No. 6249	Cap. 4950	psi
Depth	4809	feet
Inside	Clock	
Outside x	Range 12	hrs.

Initial Hydrostatic	A
Final Hydrostatic	K
Initial Flow	B
Final Initial Flow	C
Initial Shut-In	D
Second Initial Flow	E
Second Final Flow	F
Second Shut-In	G
Third Initial Flow	H
Third Final Flow	I
Third Shut-In	J

Bled to: 1361

Peterson Energy/Newport Exploration
Fassler #32-28
DST #1

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SAMPLER REPORT

Pressure in Sampler:	*	psig
Total Volume of Sampler:	2150	cc.
Total Volume of Sample:	600	cc.
Oil:	200	cc.
Water:	400	cc.
Mud:	Trace	cc.
Gas:	Trace	cu. ft.
Other:	0	

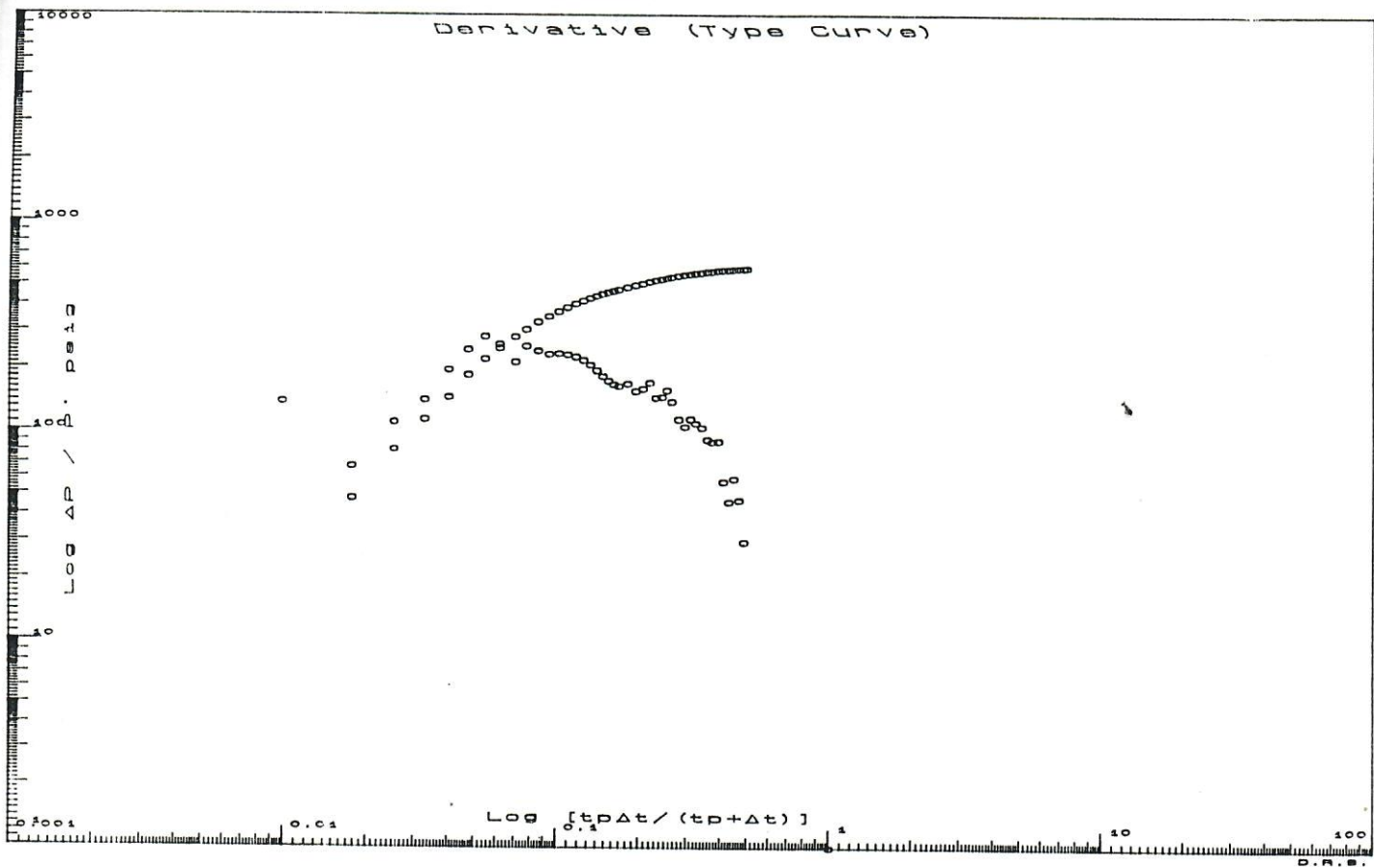
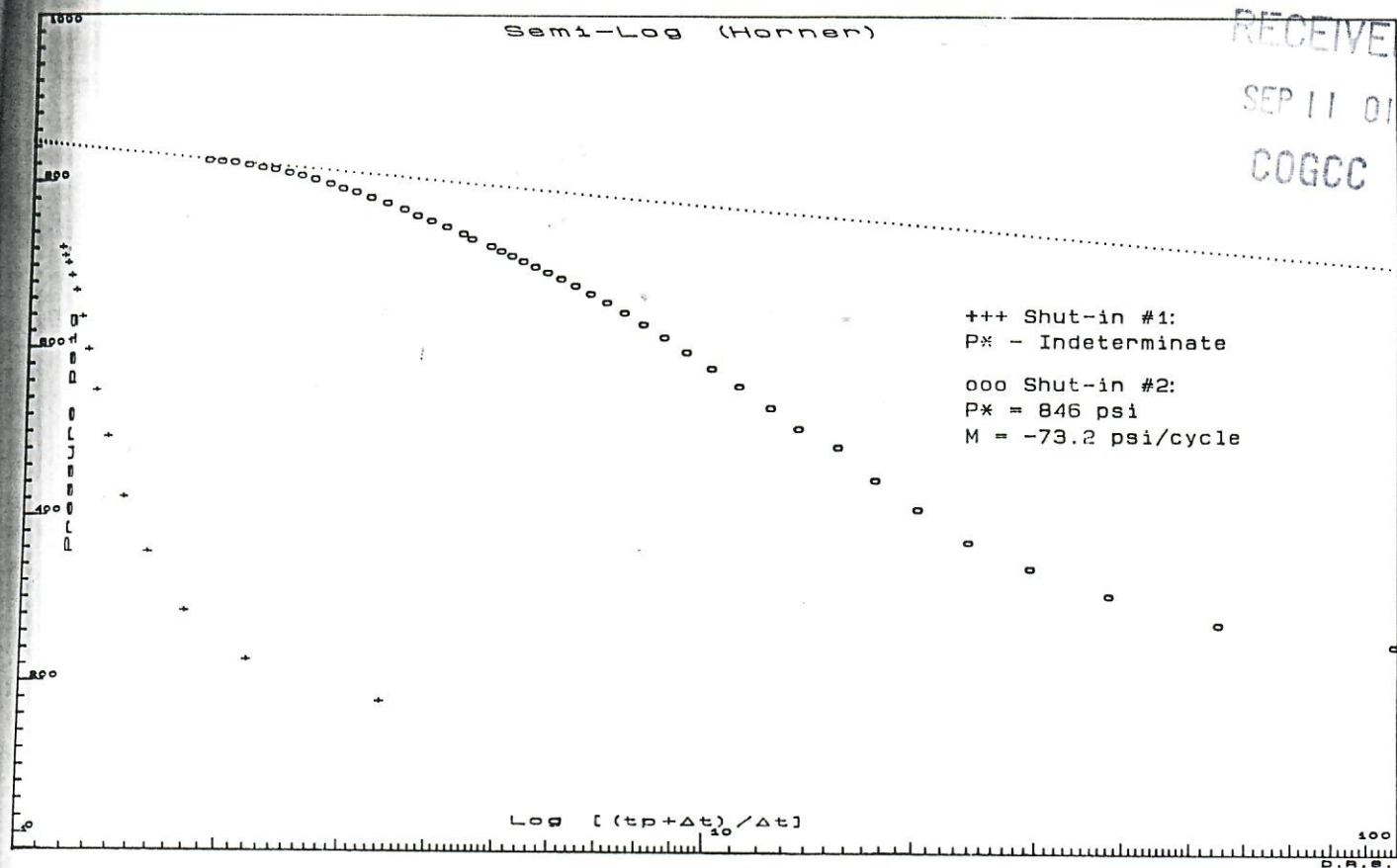
Resistivity

Make up Water	@	°F of Chloride Content	ppm.
Mud Pit Sample 2.8	@ 60	°F of Chloride Content	2,271 ppm.
Gas / Oil Ratio	Gravity	°API@	°F

Where was sample drained On Location.

Remarks: * O'ring failure caused loss of pressure.

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SEP 11 01
COGCC



Company: Peterson Energy/Newport Exploration
Well: Fassler #32-28, DST #1
Field: First Born

[Sunday: Oct. 26, 1997]
Page 1

REC #	DAY	REAL TIME	DT (HRS)	BHP (psig)
GAUGE NO. 13338 @ 4804 FT:				
BEGIN FLOW #1:				
1	0	15:44: 0	0.0000	137.38
END OF FLOW #1:				
BEGIN SHUT-IN #1:				
3	0	15:45:12	0.0000	125.69
6	0	15:46:40	0.0244	283.77
9	0	15:48: 8	0.0490	493.85
12	0	15:49:36	0.0734	636.77
14	0	15:50:48	0.0935	686.79
16	0	15:52: 0	0.1135	710.75
18	0	15:53:12	0.1335	726.37
END OF SHUT-IN #1:				
BEGIN FLOW #2:				
19	0	15:55: 8	0.0000	145.71
21	0	15:56:20	0.0199	134.02
23	0	15:57:32	0.0399	130.82
25	0	15:58:43	0.0598	130.80
27	0	15:59:55	0.0798	129.72
29	0	16: 1: 7	0.0997	131.83
31	0	16: 2:19	0.1197	133.93
33	0	16: 3:31	0.1396	137.10
35	0	16: 4:43	0.1596	140.27
37	0	16: 5:55	0.1796	144.49
39	0	16: 7: 6	0.1995	147.66
41	0	16: 8:18	0.2195	150.83
43	0	16: 9:30	0.2394	155.05
45	0	16:10:42	0.2594	158.22
47	0	16:11:54	0.2794	161.39
49	0	16:13: 6	0.2993	164.55
51	0	16:14:18	0.3193	167.72
53	0	16:15:29	0.3393	169.83
55	0	16:16:41	0.3592	174.05
57	0	16:17:53	0.3792	177.22
59	0	16:19: 5	0.3991	180.39
61	0	16:20:17	0.4191	183.55
63	0	16:21:29	0.4391	185.66
65	0	16:22:41	0.4590	188.82
67	0	16:23:52	0.4790	191.99
69	0	16:25: 4	0.4990	195.16
71	0	16:26:16	0.5189	198.32
73	0	16:27:28	0.5389	200.43
75	0	16:28:40	0.5588	203.59
77	0	16:29:52	0.5788	205.70
79	0	16:31: 4	0.5987	206.74
81	0	16:32:15	0.6187	207.79
83	0	16:33:27	0.6387	208.83
85	0	16:34:39	0.6586	209.87

[D.R.S.]

Company: Peterson Energy/Newport Exploration
Well: Fassler #32-28, DST #1
Field: First Born

[Sunday: Oct. 26, 1997]

Page 2

REC #	DAY	REAL TIME	DT (HRS)	BHP (psig)
87	0	16:35:51	0.6786	210.92
89	0	16:37: 3	0.6985	211.96
91	0	16:38:15	0.7185	211.95
93	0	16:39:26	0.7384	212.99
95	0	16:40:38	0.7584	214.03
97	0	16:41:50	0.7783	215.08
99	0	16:43: 2	0.7983	216.12
101	0	16:44:14	0.8182	216.11
103	0	16:45:26	0.8382	217.15
105	0	16:46:37	0.8582	218.19
107	0	16:47:49	0.8781	219.24
109	0	16:49: 1	0.8981	220.28
111	0	16:50:13	0.9180	220.26
113	0	16:51:25	0.9380	221.31
115	0	16:52:37	0.9579	222.35
END OF FLOW #2:				
BEGIN SHUT-IN 32:				
116	0	16:53:13	0.0000	223.41
117	0	16:53:49	0.0100	245.68
120	0	16:55:16	0.0343	337.98
123	0	16:56:43	0.0585	445.13
125	0	16:57:49	0.0767	506.54
127	0	16:58:54	0.0948	556.45
129	0	17: 0: 6	0.1149	596.88
131	0	17: 1:18	0.1349	630.06
133	0	17: 2:30	0.1549	656.39
135	0	17: 3:42	0.1750	676.68
137	0	17: 4:54	0.1950	692.57
139	0	17: 6: 6	0.2149	705.96
141	0	17: 7:18	0.2349	718.14
143	0	17: 8:30	0.2549	728.45
145	0	17: 9:42	0.2749	738.86
147	0	17:10:54	0.2949	747.18
149	0	17:12: 6	0.3149	754.46
151	0	17:13:18	0.3348	760.70
153	0	17:14:30	0.3548	767.98
155	0	17:15:42	0.3748	773.18
157	0	17:16:54	0.3947	778.37
159	0	17:18: 5	0.4147	781.49
161	0	17:19:17	0.4347	785.64
163	0	17:20:29	0.4546	788.75
165	0	17:21:41	0.4746	791.86
167	0	17:22:53	0.4945	794.97
169	0	17:24: 5	0.5145	798.08
171	0	17:25:17	0.5345	800.15
173	0	17:26:28	0.5544	803.26
175	0	17:27:40	0.5744	804.29
177	0	17:28:52	0.5943	806.36

[D.R.S.]

Company: Peterson Energy/Newport Exploration
Well: Fassler #32 28, DST #1
Field: First Born

[Sunday: Oct. 26, 1997]
Page 3

REC #	DAY	REAL TIME	DT (HRS)	BHP (psig)
179	0	17:30: 4	0.6143	808.42
181	0	17:31:16	0.6343	810.49
183	0	17:32:28	0.6542	812.56
185	0	17:33:40	0.6742	813.59
187	0	17:34:51	0.6941	814.61
189	0	17:36: 3	0.7141	815.64
191	0	17:37:15	0.7340	816.66
200	0	17:42:38	0.8238	819.72
209	0	17:48: 2	0.9136	822.77
218	0	17:53:25	1.0034	823.74

[D.R.S.]

Peterson Energy/Newport Exploration
Fassler #32-28

DISTRIBUTION OF FINAL REPORTS

Peterson Energy Mgnt, Inc. [2 + Disk]
1805 Morning Drive
Loveland CO 80538

Mr. Rick Eggleston [1]
7 Pepper Hill
Montgomery TX 77356

A.F. Gilmore Company [1]
P.O. Box 480314
Los Angeles CA 90048

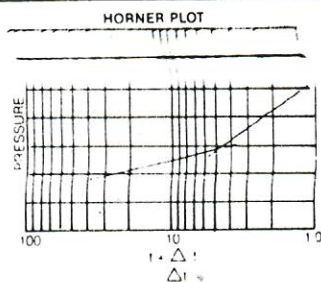
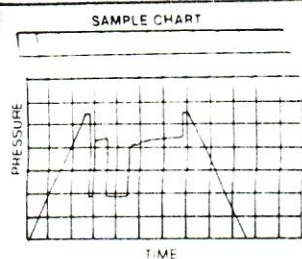
Patrick A. Doheny Living Trust [1]
136 El Camino
Beverly Hills CA 90212

Ibis Company, Limited [1]
136 El Camino
Beverly Hills CA 90212

Newport Exploration, Inc. [2]
44 Inverness Dr. East, Bldg. D
Englewood CO 80112

Peterson-Siebert Oil Co. of Texas [1]
136 El Camino
Beverly Hills CA 90212

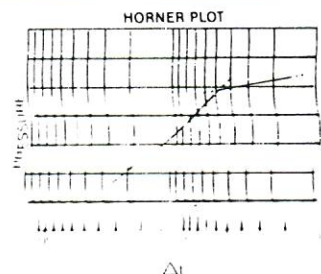
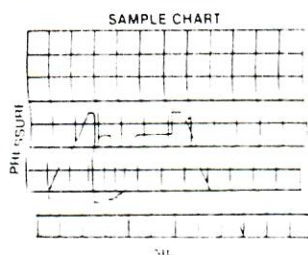
GUIDE TO DETECTION OF GEOLOGICAL ANOMALIES



Horner Plot Slope Breaks Downward

Possible Causes

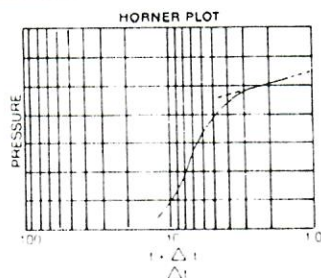
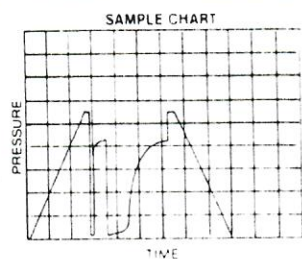
- (1) decrease in pay thickness away from the wellbore
- (2) decrease in permeability away from the wellbore
- (3) increase in viscosity of reservoir fluid (fluid contact)
- (4) barrier within the radius of investigation



Horner Plot Slope Breaks Downward

Possible Causes

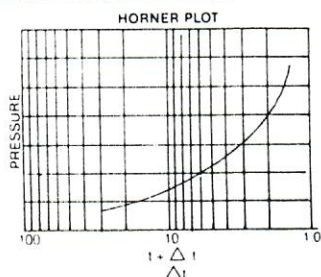
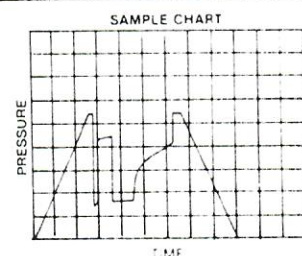
- (1) increase in pay thickness away from the wellbore
- (2) increase in permeability away from the wellbore
- (3) decrease in viscosity away from the wellbore



Early Time Deviation of Horner Plot

Possible Causes

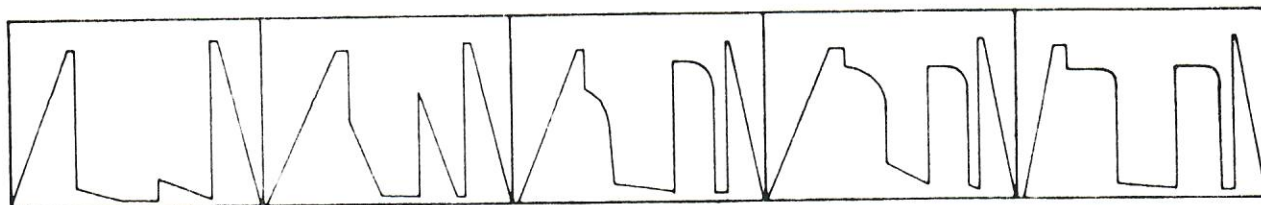
- (1) wellbore damage due to filtrate invasion, drilling solids, etc.
- (2) partial penetration of pay zone
- (3) plugging or choking of perforations (casing test only)
- (4) wellbore storage effects (low permeability gas wells)



Horner Plot Slope Continually Increasing

Possible Causes

- (1) well between two parallel boundaries (channel sand)
- (2) induced hydraulic fractures



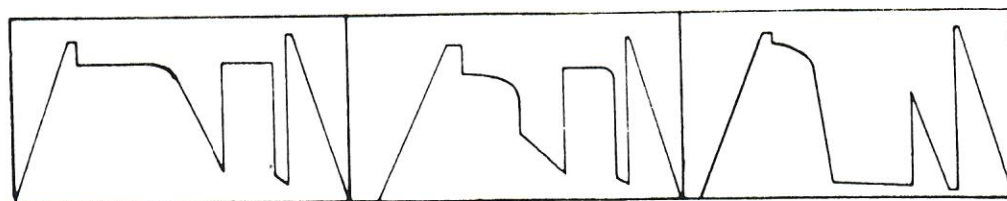
Very low permeability. Usually only mud recovered from interval tested. Virtually no permeability.

Slightly higher permeability. Again usually mud recovered.

Slightly higher permeability. Small recovery, less than 200 ft.

Average permeability. Final and initial shut-ins differ by 50 psi.

Average permeability. Strong damage effect. High shut-in pressure, low flow pressure.



Excellent permeability where final flow final shut-in pressure.

High permeability where ISIP and FSIP are within 10 psi.

Deep well bore invasion or damage. Final shut-in higher than the initial shut-in.