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Nevada Site Office  
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JAN 19 2005

John Martin, Chairman  
Board of County Commissioners  
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108 8<sup>th</sup> Street, Suite 213  
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**DRILLING NEAR THE RULISON SITE**

Reference: Ltr, Martin to Sanders, dtd, 12/08/04

This letter is in response to the above-referenced letter expressing your concerns regarding the approval of drilling permits in the vicinity of the Rulison Nuclear Test Site. I would like to assure you, we understand your concerns and have been, and continue to, monitor the situation near the Rulison Site. The Department would take every action it deemed necessary to prevent any release of radioactivity from the former test site that would have a detrimental impact on human health and/or the environment. As you may be aware, the Department of Energy (DOE) currently only controls restrictions on a forty acre area around the Rulison surface ground zero area, but the one-half mile radius you reference in your letter has been established by the Colorado Oil and Gas Conservation Commission (COGCC), in consultation with our office.

In your letter you identify three specific issues. The first dealt with a need to control the down hole location during the planned drilling. It is our understanding that the COGCC plans to include very rigorous requirements in the drilling permit to ensure the location of any hole drilled is surveyed and accurately known while the drilling is occurring. The second issue indicated a desire for the DOE to agree to "hold harmless any and all surface and water rights owners from any damage resulting from the impact of their activities upon the PRESCO well as drilled." DOE has no legal authority to offer or execute such a provision. Finally, you requested that DOE and the COGCC assure that "the security required of PRESCO will be adequate to mitigate and correct any damages to surface or water right owners that result from the drilling of the PRESCO well in the vicinity of the Rulison Project." By "security" we assume you mean financial security. DOE has no regulatory authority to require such security, but it is our understanding that part of the COGCC requirements include that a company maintain appropriate financial instruments to address any potential liability issues that may arise from their action. In addition, federal and state environmental laws and regulations address the liabilities of parties held responsible for releases of contaminants into the environment.



JAN 19 2005

The Rulison site is one of nine sites managed as part of the "Offsites" Project in the National Nuclear Security Administration Nevada Site Office Environmental Management Program. As part of our restoration activities at the Rulison site, we plan to model the transport of contaminants from the underground cavity produced as a result of the test. Our work plan for this effort is currently being reviewed by the State. However, because of the level of detail needed for such a study, this modeling effort involves doing numerous simulations using a specialized bank of computers. Part of this study will be to also evaluate the impacts from external influences, such as nearby drilling to the existing flow system. Because of the level of detail needed, this process takes time and is not scheduled to be completed until the middle of 2007. As part of this work, we will be gathering data to incorporate into the model and part of this effort will include sampling gas wells in the vicinity of the Rulison site. Currently, this sampling is scheduled to be completed by the end of April 2005.

Because of the concerns being raised over the last nine months regarding drilling near the Rulison site, we completed a more simplified modeling effort using conservative input parameters to evaluate migration of contamination from the test cavity. The results of this study indicated there would be no migration of radionuclides from the Rulison cavity to an operating gas production well located 1,500 feet away. Since this is well within the half mile radius, we have no basis to expect migration of radionuclide contamination beyond this radius. A copy of the report discussing the results of this effort is enclosed. Even with the results of this effort, it is still our intention to do the more rigorous modeling and to continue the monitoring of the Rulison Site that has been on going over the past thirty years since the test occurred.

If you have any questions, please contact Peter A. Sanders, of my staff, at (702) 295-1037.

  
Stephen A. Mellington  
Acting Assistant Manager  
for Environmental Management

ERD:PAS-1235

Enclosure:  
As stated

cc w/o encl:  
Brian Macke, COGCC  
Denver, CO



Letter Report

**Scoping Analysis of Gas Phase Transport from the  
Rulison Underground Nuclear Test**

prepared by

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Nevada Site Office  
National Nuclear Security Administration  
U.S. Department of Energy  
Las Vegas, Nevada

May 6, 2004

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The work upon which this report is based was supported by the U.S. Department of Energy under Contract #DE-AC52-00NV13609; intended for limited distribution.

## Introduction

This letter report documents the results of a computer model to quantify the travel time of tritium (radioactive hydrogen) from an underground nuclear detonation in 1969 toward a proposed producing gas well located 1,500 feet (457 meters) away. The nuclear detonation was the result of a joint program between the U.S. Atomic Energy Commission (predecessor to the Department of Energy, DOE) and the petroleum industry to develop technology for nuclear stimulation of low permeability gas reservoirs not conducive to production by conventional means. Project Rulison was the second experiment under the program.

The Rulison site is located in west-central Colorado, approximately 64 km northeast of Grand Junction. A 40-kiloton nuclear explosive was placed at a depth of 2,568 m below the land surface in well R-E (also recognized as the Hayward #25-95 (R-E)) located in the NE1/4SW1/4 Section 25, T7S, R95W, 6<sup>th</sup> P.M. in Garfield County. The detonation was within the Williams Fork Formation of the Mesaverde Group and occurred on September 10, 1969.

## Conceptual Model of Gas Flow and Radionuclide Transport

Figure 1 shows the model domain in two-dimensions. A proposed gas well located 457 m from the R-E well would pump gas with a specified decline curve over a 30-year period. Production from this well induces both gas and liquid water flow through the Williams Fork Formation. Although the details of the well depth and production intervals are not known a priori, it is possible that the well would produce from a zone at the same depth of the detonation, which is assumed in the model. It is also assumed that the well will have multiple hydraulically fractured zones in the Williams Fork Formation, per current practice in the region. The hydraulically fractured, perforated interval at the nuclear test horizon is assumed to be 6.1 m thick (20 feet). The ambient pressure gradient is assumed to be much less than the gradient induced by pumping and is therefore assumed to be zero.

Flow is assumed to be largely horizontal as it is controlled entirely by the pumping well and the high-permeability fracture zone. Therefore, a reservoir thickness of 103 m was simulated, which was determined from the assumed multiple depths for the hydraulic fracturing. The simulation domain was organized such that the hydraulic fracturing would vertically straddle the formation, and that this depth was exactly opposite the detonation depth. The extent of the hydraulic fracture is assumed as 68 m vertically and 88 m horizontally away from the well and the intrinsic permeability of the fracture zone was estimated as  $2.96 \times 10^{-14} \text{ m}^2$  (30 millidarcy; md) with a porosity of 0.15 (Keith Blair, Presco, Inc., personal comm.). Intrinsic permeability of the undisturbed formation is  $7.90 \times 10^{-18} \text{ m}^2$  (0.008 md) and the porosity is 0.112. These values were determined from the mean values reported by Frank (1971). Gas saturation throughout the formation (including the hydraulically fractured zone and the fracture zone associated with the nuclear stimulation) was estimated as 0.6 (Keith Blair, Presco, Inc., personal comm.). The permeability was allowed to change as a function of the volumetric gas saturation. The van Genuchten equations were used for both relative permeability and capillary pressure. The corresponding parameters (residual saturation, van Genuchten parameters  $m$ ,  $n$  and  $\alpha$ ) were from Carsel and Parrish (1988). Although developed for soils, relationships for a silty clay loam were used (as this texture has the lowest intrinsic permeability of their soil types) and scaled to the intrinsic permeabilities appropriate for the Williams Fork Formation. The simulations are not very

sensitive to the choice of relative permeability and capillary pressure functions as the gas content changed little throughout time and throughout the model domain.

The fracture zone around the nuclear detonation was assumed to be 98 m tall and 238 m wide. The permeability is unknown – we assumed it to be the same as that of the zone of hydraulic fracturing around the production well ( $2.96 \times 10^{-14} \text{ m}^2$ ).

The outer, vertical boundary condition (1,000 m away from the well) was prescribed as the formation pressure 21.87 MPa (3156 psi; Keith Blair, personal comm.). The horizontal boundary conditions above and below the simulation domain were prescribed as zero flux; this is to constrain flow largely to the horizontal direction and not allow for flow from the boundaries. This is considered an accurate physical description, as there are perforated/fractured zones above and below the one that is simulated, which would result in a horizontal streamline between adjacent perforated intervals in which no flow would cross. The boundary condition at the producing well was prescribed flux corresponding to the decay curve supplied by Presco, Inc.

### **Numerical Model**

The TOUGH2 (Transport of Unsaturated Groundwater and Heat) integral finite difference simulator was used to implement the model as it handles three-dimensional, multiphase, multicomponent heat and mass transport through porous media in a fully coupled manner (Pruess *et al.*, 1999). The code fully accounts for the movement of gaseous and liquid phases, their transport of latent and sensible heat, and phase transitions between liquid and vapor occurring under pressure, viscous, capillary, and gravity forces according to Darcy's law. The program provides options for specifying injection or withdrawal of energy (heat) and fluids. The equation of state module that was implemented (EOS7R) is capable of handling four components: water, air, solute and heat (although only isothermal flow was simulated). TOUGH2 is a DOE-sponsored code that has been used extensively to study heat and mass flow in geothermal reservoirs, saturated/unsaturated zones, and oil and gas reservoirs.

Several changes were made to the TOUGH2 program in order for it to correctly simulate the important processes. The EOS7R module assumes the gas phase to be air and air/water mixtures. This was easily changed to replace air properties with those of methane, which are important in the density and viscosity correlations. No changes were required with respect to phase partitioning. Values for Henry's constant of methane dissolution in water vary between  $4.41 \times 10^{-10} \text{ Pa}^{-1}$  (0°C) to  $1.41 \times 10^{-10} \text{ Pa}^{-1}$  (100°C). Since the values change by only a factor of three, and because the geothermal gradient relates to a temperature ~100°C throughout much of the reservoir, the default value for air dissolution in water was used ( $10^{-10} \text{ Pa}^{-1}$ ). This is not expected to have a significant effect on results, as the dissolution of methane in water is small.

In addition to radioactive decay, tritium fractionates isotopically between the liquid and gas phases. Fractionation is the preferential partitioning of an isotope (as opposed to a molecule, as described above) between the gas and liquid phases. (There is also fractionation within a phase, for example, tritium in water vapor and methane, but this has no effect on transport. Similarly, tritium fractionation between liquid water and water vapor is small due to the small amount of water vapor in the vapor phase.) Tritium will preferentially fractionate between phases to form tritiated methane gas,  $\text{C}^3\text{HH}_3$ , and tritiated liquid water,  $^3\text{HHO}$ . The

gas phase will favor light isotopes of methane ( $^1\text{H}$ ) while the liquid phase will favor heavier isotopes ( $^3\text{H}$ ). TOUGH2 does not handle isotope fractionation under equilibrium conditions. Implementation of isotope fractionation was begun in the TOUGH2 equation-of-state module (EOS7R), although it has not been fully tested. For this reason, fractionation of tritium between liquid water and methane was not included in these simulations, although it will be included in the full Rulison modeling project to begin in FY05. The results are still accurate, as fractionation acts to change concentrations by about a factor of two (the fractionation factor for tritium between methane and liquid water). Since the concentration field varies over ten orders of magnitude, the effect is not noticeable on the results. In addition, this uncertainty is well within the uncertainty in permeability, which is probably on the order of several orders-of-magnitude.

Initial conditions are presented in Table 1. The problem was formulated as two-dimensional axisymmetric flow to a well. The solution domain was 1,000 m long ( $x$ -direction) by 103 m high ( $z$ -direction). The initial source was estimated as 3,176 Curies (Ci) mixed with 30 bbls ( $4.769 \times 10^9$  gr  $\text{H}_2\text{O}$ ) of water (Reynolds *et al.*, 1970). This assumes that 40% of the tritium was amalgamated into the melt, which was the estimate at the Rio Blanco nuclear stimulation site (Toman and Tewes, 1972). This has decayed for 35 years; the amount remaining after this decay is calculated from the solution to  $dM/dt = -\lambda M$  where  $M$  is the initial mass and  $\lambda$  is the decay constant (defined as  $\lambda = \ln 2 / T_{1/2}$  where  $T_{1/2}$  is the radioisotope half-life). After nearly three half-lives ( $T_{1/2}$  for tritium is 12.26 years), the radioactivity

Table 1. Initial conditions for simulations.

Parameter	Value	Source
Intrinsic permeability of undisturbed formation, $\text{m}^2$	$7.90 \times 10^{-18}$	Reynolds <i>et al.</i> , 1970 and Presco, pers. comm.
Intrinsic permeability of hydraulic fracture zone, $\text{m}^2$	$2.96 \times 10^{-14}$	Keith Blair, Presco
Intrinsic permeability of nuclear stimulated zone, $\text{m}^2$	$2.96 \times 10^{-14}$	Assumed same as hydraulic fracture zone
Porosity, undisturbed	0.112	Various reports
Porosity, hydraulic fracture	0.15	Keith Blair, Presco
Porosity, nuclear stimulated zone	0.15	Assumed same as hydraulic fracture zone
Relative permeability	van Genuchten func.	Carsel and Parrish, 1988
Capillary pressure curve	van Genuchten func.	Carsel and Parrish, 1988
Reservoir Pressure, Pa	21.87 MPa	Toman, 1975
Gas saturation	0.6	CER Geonuclear; Toman and Tewes, 1972
$^3\text{H}$ radioactivity, Ci	1447	Reynolds <i>et al.</i> , 1970
Diffusion coefficient, $^3\text{H}$ in methane, $\text{m}^2 \text{s}^{-1}$	$7.26 \times 10^{-5}$	Cussler, 1997
Diffusion coefficient, $^3\text{H}$ in liquid water, $\text{m}^2 \text{s}^{-1}$	$3.47 \times 10^{-9}$	Mills, 1973
Diffusion coefficient, He in methane, $\text{m}^2 \text{s}^{-1}$	$6.75 \times 10^{-5}$	Cussler, 1997
Diffusion coefficient, He in liquid water, $\text{m}^2 \text{s}^{-1}$	$6.28 \times 10^{-9}$	Cussler, 1997
Diffusion coefficient, $\text{CH}_4$ in liquid water, $\text{m}^2 \text{s}^{-1}$	$1.49 \times 10^{-9}$	Cussler, 1997
$^3\text{H}$ half-life, yr	12.26	Parrington <i>et al.</i> , 1996

Diffusion coefficients measured or estimated for 25°C

is 0.138 of the initial value. Therefore, the initial radioactivity for the simulations (i.e., assuming that pumping began in 2004) is 439 Ci. The initial concentration is therefore is  $3.4 \times 10^7$  pCi/l in the liquid phase. The tritium radioactivity at the start of the simulations (439 Ci) calculates to a mass fraction of tritium in the liquid phase (the input format for TOUGH2) of  $9.59 \times 10^{-12}$ . The simulator then partitions tritium between the liquid and gas phases in the first time step based upon Henry's law.

The decline curve (provided by Keith Blair, Presco, Inc.) is presented in Table 2. The decline curve is for a well typically producing from ten 20-ft zones. Therefore, the values were divided by ten (since the model simulates production from one zone) and converted to  $\text{kg sec}^{-1}$  for each month (assuming a constant gas density of  $0.625 \text{ kg m}^{-3}$ ). The well was estimated to produce for 30 years; the final value in the table was kept constant for the remaining 20 years of production.

Table 2. Typical decline curve for simulations. Values are in thousands of cubic feet of gas (MCFG) for the entire month.

Year	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1992	39,000	35,400	31,350	24,000	21,000	18,600	16,500	15,900	15,000	14,400	14,100	13,950
1993	11,550	11,550	11,550	10,800	10,800	10,800	10,260	10,260	10,260	9,750	9,750	9,750
1994	9,000	9,000	9,000	8,250	8,250	8,250	7,860	7,860	7,860	7,500	7,500	7,500
1995	7,050	7,050	7,050	6,600	6,600	6,600	6,450	6,450	6,450	6,300	6,300	6,300
1996	6,150	6,150	6,150	6,000	6,000	6,000	5,850	5,850	5,850	5,700	5,700	5,700
1997	5,550	5,550	5,550	5,400	5,400	5,400	5,250	5,250	5,250	5,100	5,100	5,100
1998	4,950	4,950	4,950	4,800	4,800	4,800	4,710	4,710	4,710	4,650	4,650	4,650
1999	4,560	4,560	4,560	4,500	4,500	4,500	4,380	4,380	4,380	4,260	4,260	4,260
2000	4,140	4,140	4,140	4,050	4,050	4,050	3,900	3,900	3,900	3,810	3,810	3,810
2001	3,690	3,690	3,690	3,600	3,600	3,600	3,450	3,450	3,450	3,300	3,300	3,300

The TOUGH2 simulator was run with variable time stepping; an initial time-step of 1 second was allowed to increase to a maximum of  $10^9$  seconds. The convergence criterion for relative error was set at  $10^{-5}$  for all simulations. Precision was checked by running several simulations with the relative error set at  $10^{-6}$ ; the difference in results was not discernible.

## Results and Discussion

Figure 2a shows the initial condition. The tritium source is located 458 m from the proposed pumping well. Figure 2b, c, and d show gas phase concentrations at 10 years, 25 years, and 35 years after the detonation. Transport of tritium in the gas phase is due solely to diffusion, as pumping does not begin until 35 years after the detonation (the length of time between the detonation and pumping of the proposed well in the year 2004). The slight asymmetry of the concentration field is due to the nonuniform gridding scheme on either side of the source. Figures 3a, 3b, and 3c show tritium concentrations in the gas phase for 45 years, 55 years, and 65 years after the detonation (corresponding to 10, 20, and 30 years of pumping, respectively). Results show that for these initial and boundary conditions, a concentration of 1 pCi/L nearly reaches the drilling exclusion zone after 10 years of

pumping. Figure 3d shows mass fraction of tritium in the liquid (water) phase. The contours are bounded at the low end by the same value,  $1.04 \times 10^{-19}$ , which is equivalent to 1 pCi per liter. The uppermost values are different: since tritium partitions differently in liquids and gases, the upper value is the maximum amount that each phase could contain based upon the initial mass fraction. For the most part, tritium migration is unaffected by pumping and controlled by diffusion in the gas phase, as the pumping rate is so low. After 30 years of pumping, the edge of the tritium "plume" has traveled approximately 180 meters, but is still 280 meters from the production well.

Figures 2 and 3 show that the center of the plume remains stationary, while the tritium radioactively decays. The radioactive decay is most obvious in the decline in concentration at the center of the plume, but decay is also responsible for the slowing of the growth of the plume. Note that there is little lateral migration from 45 years after the Rulison test.

Figure 4 is a similar simulation, but with radioactive decay turned off. Results are shown for 10, 20, and 30 years of pumping. This is what would be expected for a radionuclide with a very long half-life or some other, stable, constituent. The tritium mass fraction fields are similar to those of Figure 3, although they extend about 100 m farther in all directions. The difference between Figures 3 and 4 is due to the effect of radioactive decay on reducing the tritium mass shown in Figure 3. In both cases, diffusion is the process controlling tritium migration, as seen by the fairly uniform concentration fields.

To see the effect of pumping, the pumping rate was increased to a constant value of  $0.1 \text{ kg sec}^{-1}$  (one order of magnitude greater than the highest pumping rate input for the decline curve). Figure 5 shows the results of a simulation with a single permeability of  $2.96 \times 10^{-14} \text{ m}^2$  throughout the domain. This permeability is the same as that given to the fracture zones around the producing well and the emplacement hole R-E. Flow is seen to sweep throughout the domain, carrying tritium in the gas phase. The tritium concentration field in the liquid phase shown in Figure 5d corresponds with the concentration field in the gas phase, although not due to liquid phase (water) movement. Rather, the tritium component of the gas phase is in constant equilibrium with the liquid phase (e.g., Henry's law partitioning) and therefore becomes dissolved in the gas phase due to its volatility and not due to liquid-phase transport per se.

## References

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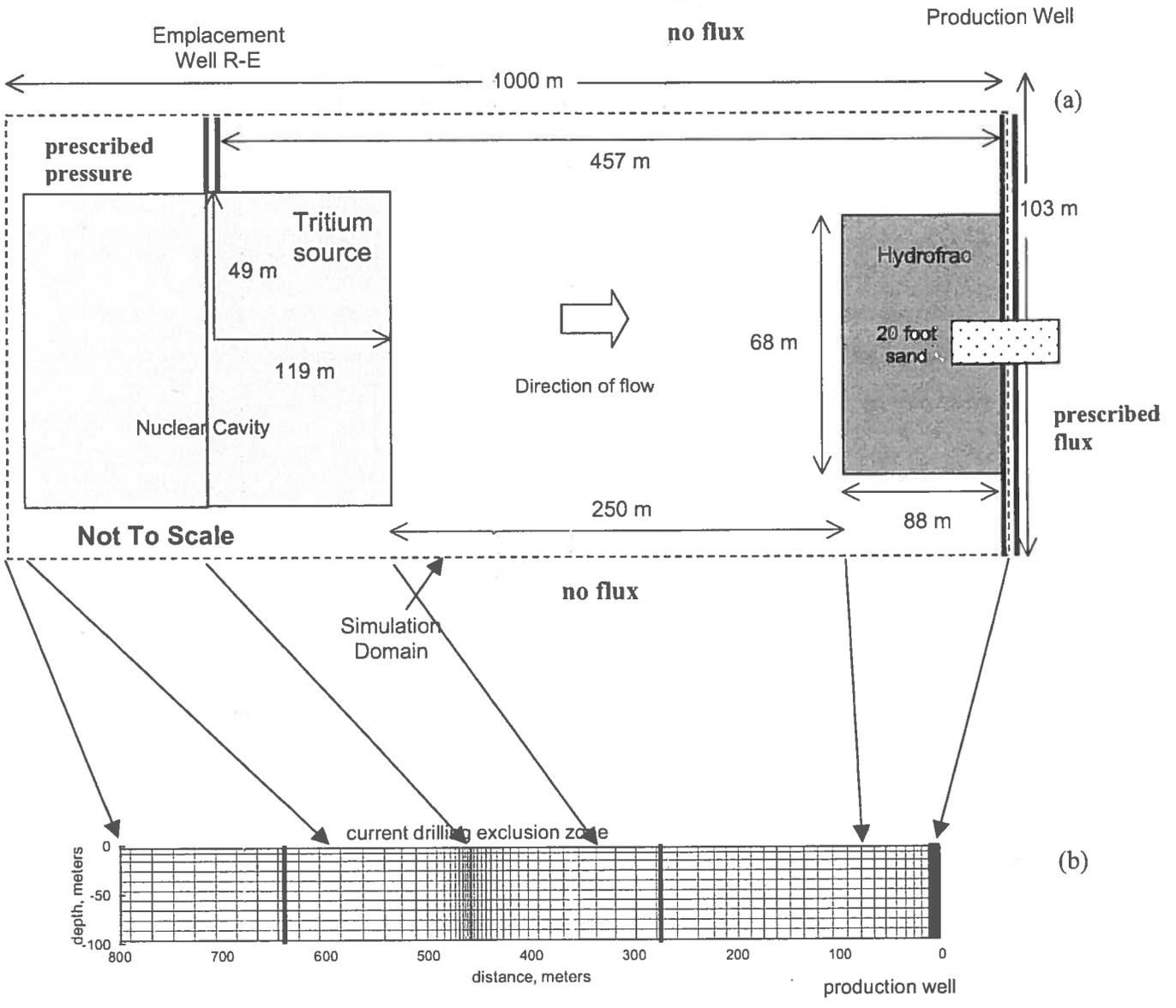


Figure 1. Model formulation for gas flow and tritium transport to a pumping well (a), and integral finite difference grid for simulations (b).

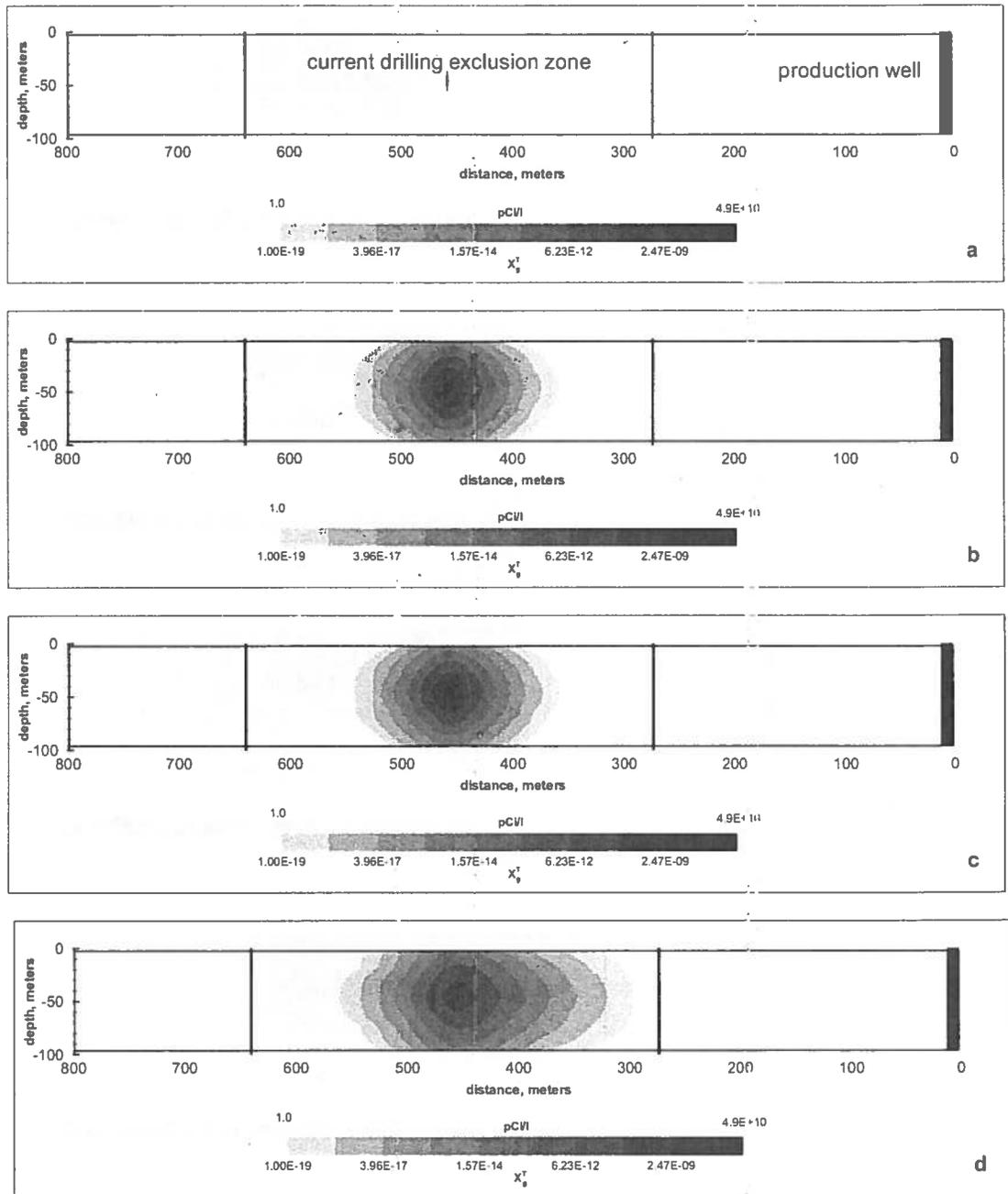


Figure 2. Tritium concentration in the gas phase as mass fraction (kg tritium / kg gas) and picoCuries per liter at (a) the start of the simulation, (b) 10 years, (c) 25 years, and (d) 35 years after the nuclear detonation. The heavy vertical bars show the limit of the current drilling exclusion zone:

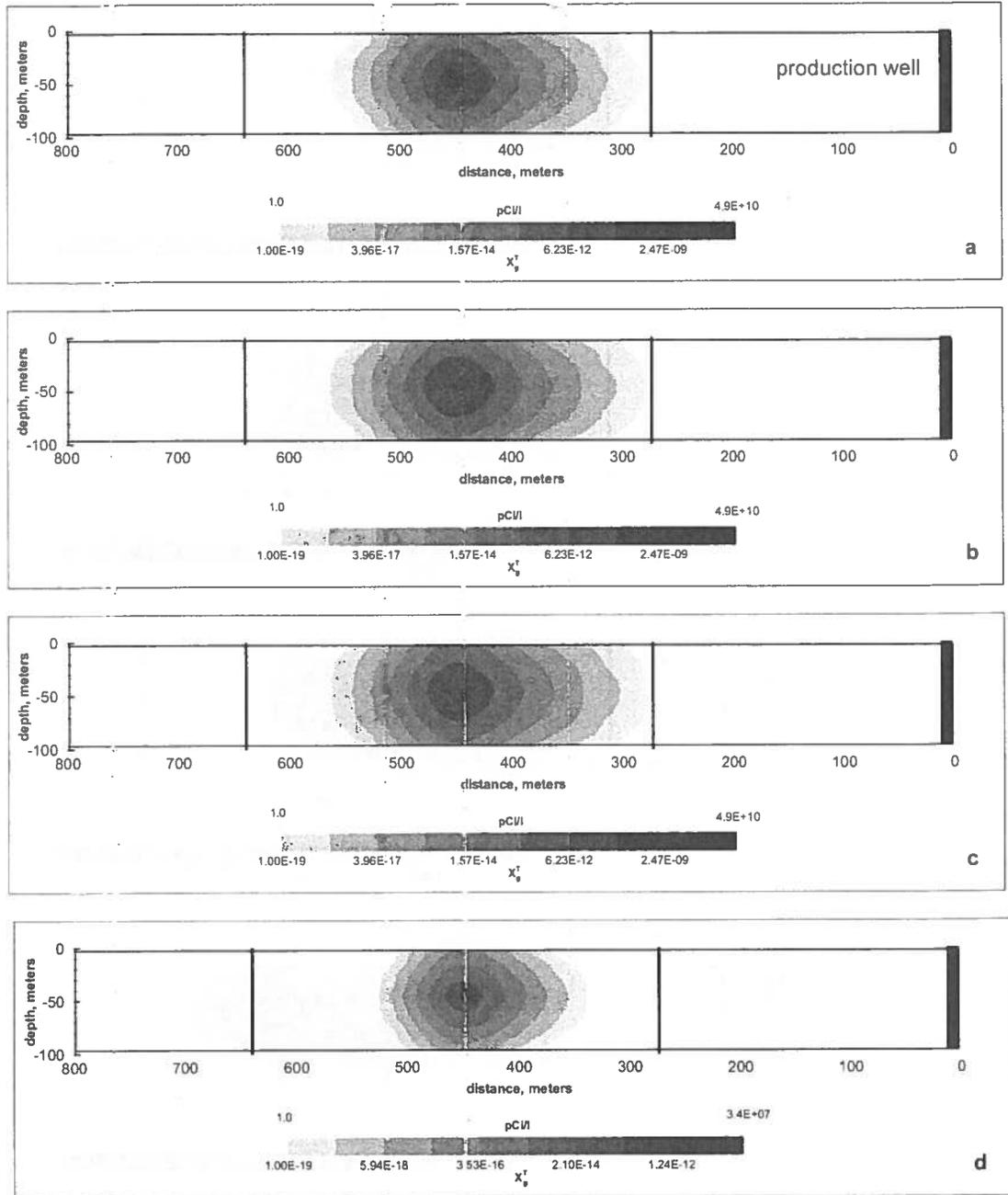


Figure 3. Tritium concentration in the gas phase for the same simulation as in Figure 2 at (a) 45 years, (b) 55 years, (c) and (d) 65 years after the nuclear detonation. Pumping began 35 years after the detonation. Figure (d) shows the concentration of tritium in the liquid phase 65 years after the detonation.

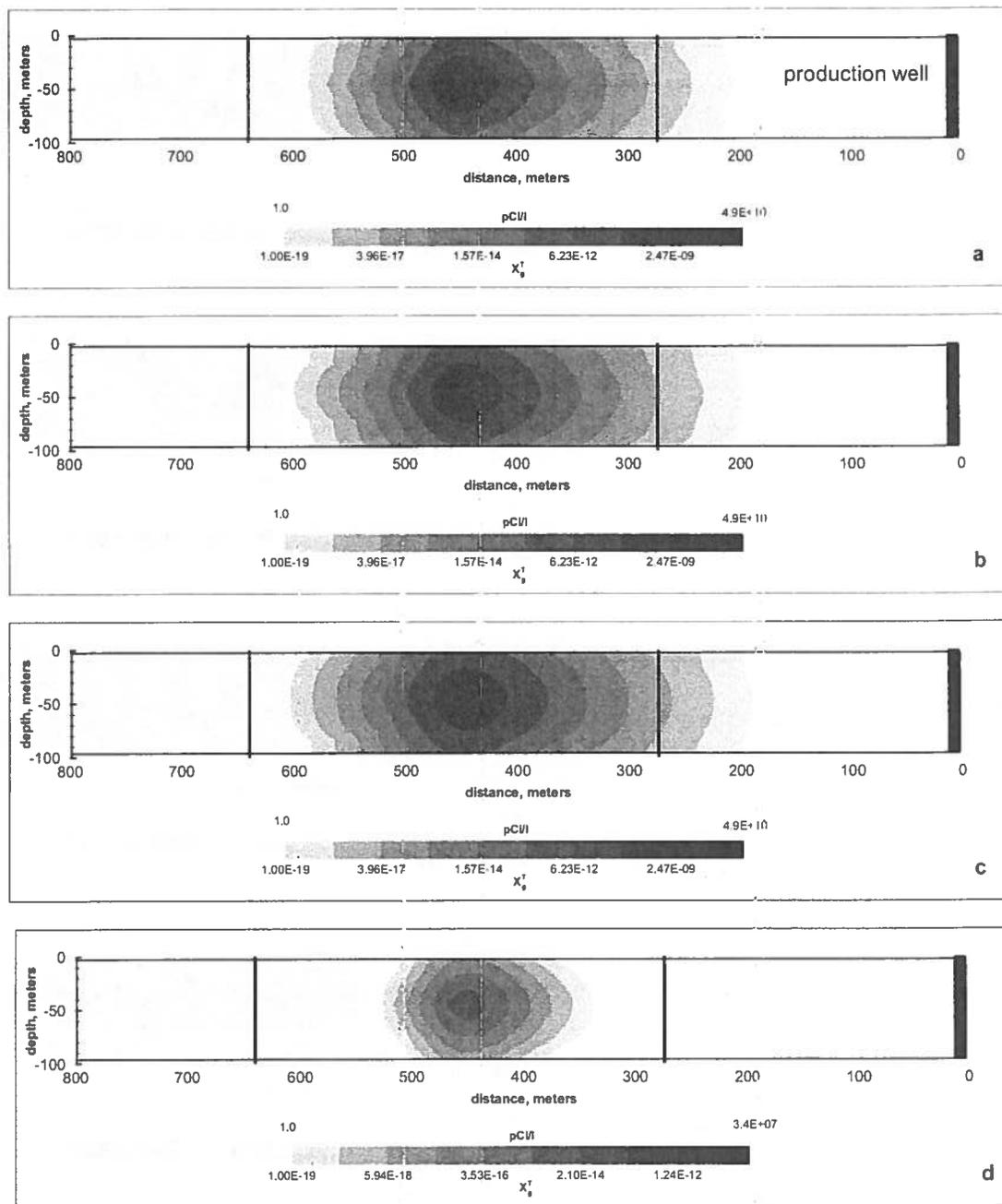


Figure 4. Tritium concentration in the gas phase after (a) 45 years, (b) 55 years, and (c) 65 years after the detonation with no radioactive decay. Figure (d) is the concentration of tritium dissolved in the liquid phase after 65 years.

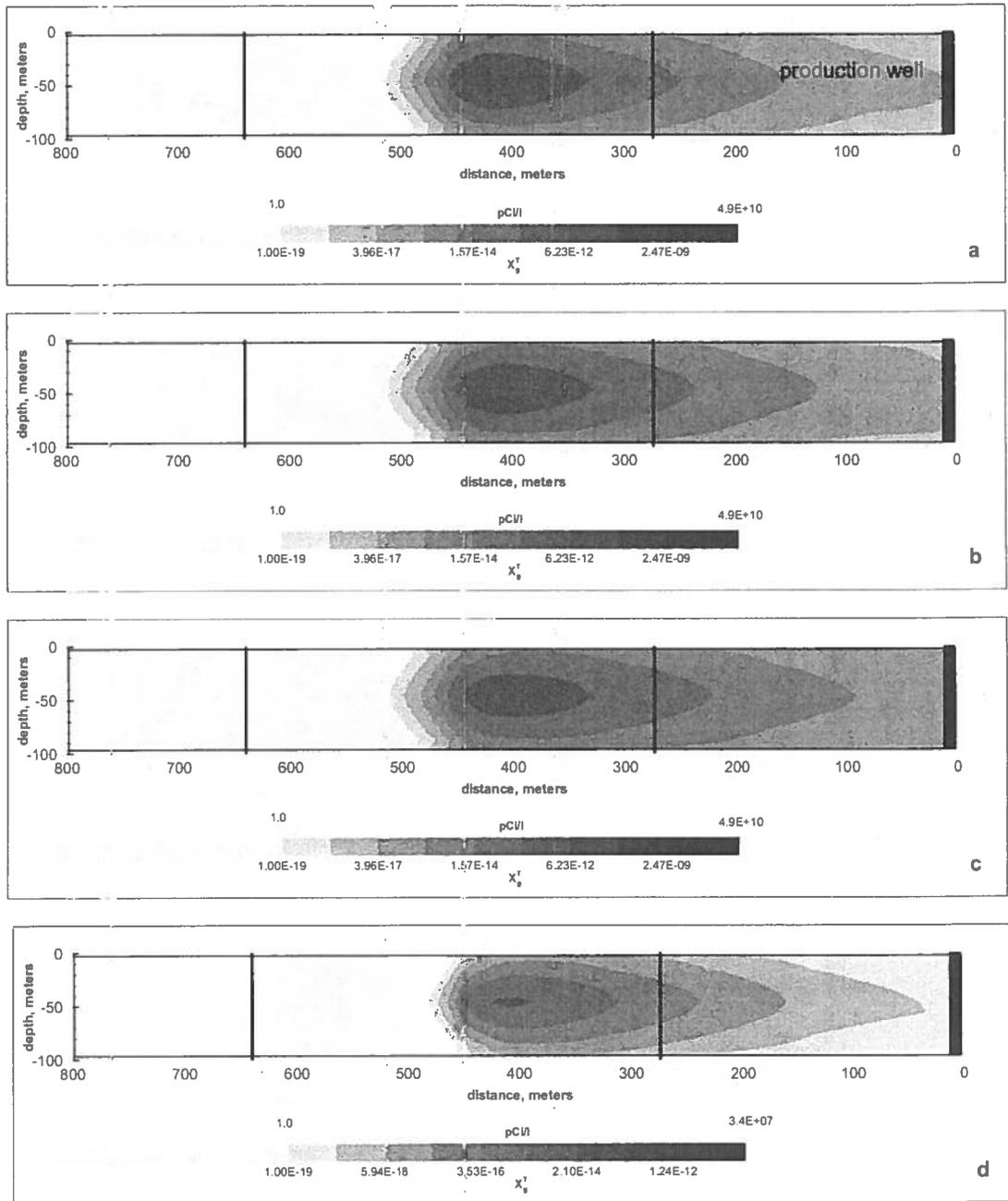


Figure 5. Tritium concentration in the gas phase after (a) 45 years, (b) 55 years, and (c) 65 years, after the detonation, with radioactive decay. Figure (d) shows tritium concentration in the liquid phase 65 years after the nuclear detonation. This simulation is different than those in the previous figures as the domain is homogeneous with  $k=2.96 \times 10^{-14} \text{ m}^2$  and the pumping rate is constant at  $0.1 \text{ kg sec}^{-1}$ .