

# FINAL DRAINAGE REPORT

## BULLDOG #5-31H-790 COMPLETION PIT

---

### MOFFAT COUNTY, COLORADO

**PREPARED FOR:**  
AXIA ENERGY INC.  
1430 LARIMER STREET, SUITE 400  
DENVER, CO 80202  
PH: (720) 746-5200  
CONTACT: JESS PEONIO

**PREPARED BY:**  
OLSSON ASSOCIATES  
826 21 ½ ROAD  
GRAND JUNCTION, CO 81505  
PH: (970) 263-7800  
CONTACT: LORNE C. PRESCOTT  
WYATT E. POPP, PE, LEED AP

**JULY 9, 2012**

**OLSSON ASSOCIATES  
PROJECT No. 012-1222**

ENGINEER'S STATEMENT

I hereby certify that this *Final Drainage Report* for the design of Axia Energy Inc., Bulldog #5-31H-790 Completion Pit was prepared by me, or under my direct supervision, in accordance with the provisions of the *Stormwater Management Manual* for the owners thereof. I understand that Moffat County does not and will not assume liability for drainage facilities designed by others.

Wyatt E. Pope, P.E.  
Registered Professional Engineer  
State of Colorado, No. 38514



7/11/12  
Date

OWNER'S STATEMENT

I, J. Peonio / Axia Energy, hereby certify that the drainage facilities for Axia Energy Inc., Bulldog #5-31H-790 Completion Pit shall be constructed according to the design presented in this report. I understand that Mesa County does not and will not assume liability for the drainage facilities designed and/or certified by my engineer. I understand that Mesa County reviews drainage plans but cannot, on behalf of Axia Energy Inc., Bulldog #5-31H-790 Completion Pit, guarantee that final drainage design review will absolve \_\_\_\_\_ and/or their successors and/or assigns of future liability for improper design. I further understand that approval of the Final Plat and/or Final Development Plan does not imply approval of my engineer's drainage design.

Axia Energy, LLC  
Owner/Developer

J. Peonio  
Authorized Signature

7/11/12  
Date

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## I. INTRODUCTION

### A. Background

This Final Drainage Report has been prepared for Axia Energy LLC, Bulldog #5-31H-790 Completion Pit (the SITE) by Olsson Associates. This report evaluates the SITE's historic drainage patterns, analyzes the change in stormwater quantity/quality associated with existing development, and provides design to alleviate the impacts of increased stormwater runoff due to the proposed development.

### B. Project Location

The SITE is located in the NW  $\frac{1}{4}$  of the NE  $\frac{1}{4}$  of Section 5, Township 7 North, Range 90 West of the Sixth Principal Meridian, County of Moffat, State of Colorado. Refer to Figure 1 for project location.

The SITE is approximately 5.5 miles north of the town of Craig, Colorado on County Road 112. County Road 112 is located approximately 0.85 miles west of the site, and County Road 22 is located approximately 1.6 miles to the south.

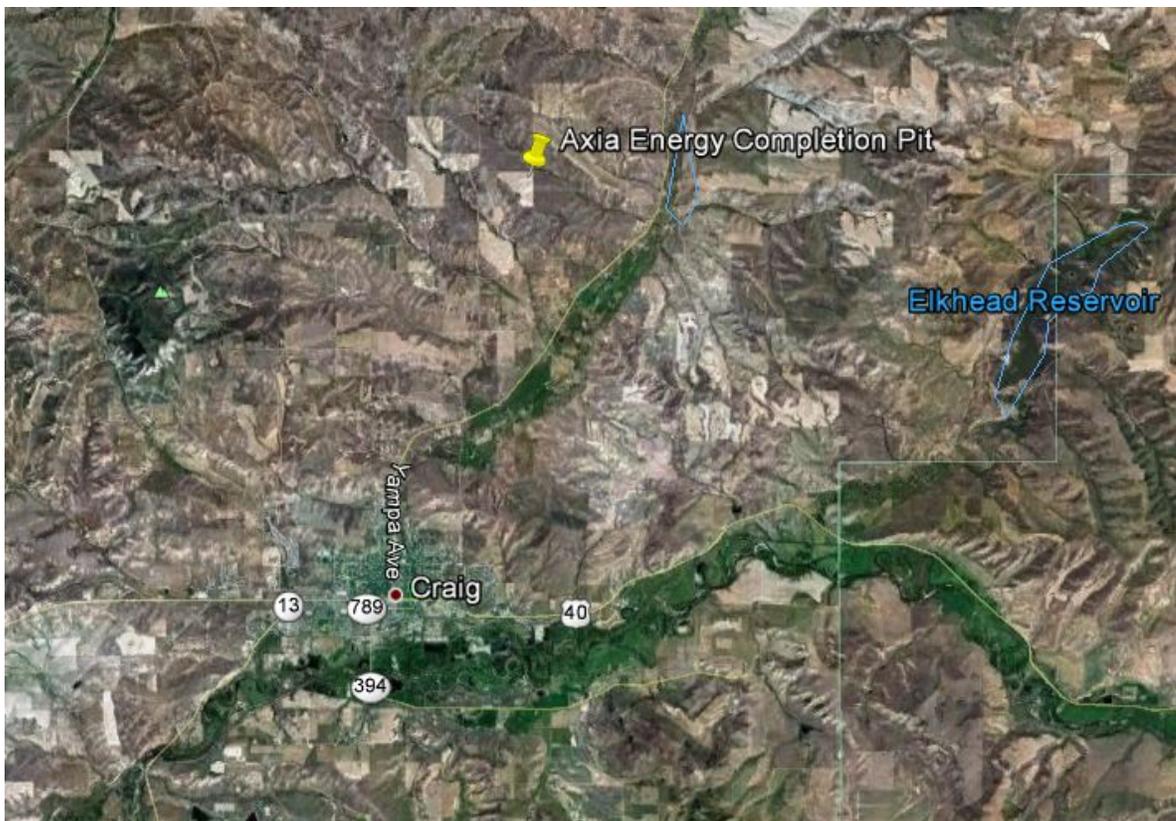


Figure 1: Vicinity Map

### C. Property Description

The SITE consists of a total disturbance around 3.4 acres which consists of a completion pit graded into hilly terrain and an access road turnaround. Prior to development, the SITE is covered by native vegetation, and sheet flows from southwest to northeast.

According to the NRCS Web Soil Survey, soils in the area of the SITE consist of Forelle loam on 3 to 12% slopes, which are classified as hydrologic group Type B. A soil map and description of NRCS soil groups from NRCS is included within Appendix A.

### D. Previous Investigations

To our knowledge, no previous drainage studies have been approved for the SITE.

## II. DRAINAGE SYSTEM DESCRIPTION

### A. Existing Drainage Conditions

The SITE drains to Coon Gulch to the northeast which eventually empties into Fortification Creek to the east. Refer to the General Location Map in Appendix A for the SITE location relative to major tributary drainage ways.

The SITE generally slopes from the southwest to the northeast at approximately 4.0% to 7.0% slope. The SITE generally drains via overland flow to existing swales which flow to Coon Gulch. The Rational Method for determining runoff per the Colorado Floodplain and Stormwater Criteria Manual (the MANUAL) and the Urban Drainage and Flood Control District's *Urban Storm Drainage Criteria Manual* has been applied resulting in Historic peak flow rates listed in Table 1, and calculations of each flow rate are presented in Appendix B.

**Table 1: Historic Peak Runoff**

Drainage Basin	Area (Ac)	25-YR Peak Flow (cfs)	100-YR Peak Flow (cfs)
NORTH - Swale on the north side of Completion Pit	2.93	1.94	3.38
SOUTH - Swale on the south side of Completion Pit	0.19	0.16	0.27
CP – Completion Pit Area	2.82	2.22	3.87

### B. Master Drainage Plan

To our knowledge, no master drainage studies have analyzed the SITE.

### C. Offsite Tributary Area

The SITE will not be adversely affected by stormwater from adjacent land. The offsite run-on will be diverted around the site by proposed grass lined drainage swale and released. For the purposes of this study, all adjacent land was assumed to remain undeveloped in the

foreseeable future.

An access road will be constructed across an existing channel. A culvert will be designed to handle the 100-YR flow from the tributary area draining to this point. Calculations are shown in Appendix C.

During construction, run-off from the SITE should be treated prior to leaving the SITE using methods described in Vol. 3 of the Urban Drainage and Flood Control District's Urban Storm Drainage Criteria Manual, including use of straw bales and/or other methods to provide temporary water quality.

#### D. Proposed Drainage System Description

Three basins were used to model the SITE and existing run-on. Stormwater generated by the existing run-on will be collected in two grass lined drainage swales on the north and south sides of the Completion Pit. The drainage swales will direct stormwater around the Completion Pit and discharge along the north and south corners of the SITE. The proposed access road across the north swale will be conveyed under the road via a culvert.

Drainage Basin	Area (Ac)	25-YR Peak Flow (cfs)	100-YR Peak Flow (cfs)
NORTH	2.93	1.92	3.35
SOUTH	0.19	0.14	0.24
CP*	2.82	7.92	10.30

\*CP – Completion Pit facility will not release stormwater.

The Completion Pit will be rectangular, approximately 19'-7" deep with 2:1 side slopes. The dimensions will be 250'x400' at the top of the embankment, which is at elevation 6519.00', providing 2'-0" of freeboard height. Access to the detention pond for maintenance can be provided on the north portion of the embankment.

The Completion Pit will provide storage for 206,198 Barrels of used water at the maximum design elevation of 6517.0'. The pond will not release any water and will not have an outlet structure or overflow spillway. Stormwater captured by the water impoundment pond will not be discharged onto the existing adjacent property. The waters contained within the completion pit will be trucked in and out. The pond will be self-contained and lined with a single impervious HDPE liner and will be equipped with a leak detection system. The bottom of the pond has a 1% slope swale to facilitate draining, and the bottom is sloped at 2% to the swale.

The pond will not be considered jurisdictional, as the maximum difference in height between the embankment and existing ground is 9.5 feet. Without any outlet structure or overflow spillway, the definition of a jurisdictional embankment height becomes 10 feet or more from the top of the embankment to the existing ground.

The drainage swales will be triangular in shape, 6 feet wide, 1 foot deep, with side slopes of 3:1. The swales have a capacity of 15 cfs at a 3% slope, which is more than adequate to convey the 100-year off-site stormwater flows. Although larger than necessary, swales of

any smaller size become difficult to construct and maintain.

Refer to Appendix B for developed condition hydrologic calculations and Appendix C for hydraulic calculations.

#### **E. Drainage Facility Maintenance**

The owner shall be responsible for maintaining all on-site drainage facilities. A minor amount of continuous maintenance will be necessary to keep vegetation established and the leak detection system working in its original designed capacity. Although the completion pit is not meant for stormwater, the pond bottom should be scraped and regraded as needed to remove sediment build-up. In addition, the pond should be examined after any significant rainfall event to ensure proper functionality.

### **III. DRAINAGE ANALYSIS AND DESIGN CRITERIA**

#### **A. Regulations**

This report has been prepared in accordance with criteria set forth in the MANUAL and the Urban Drainage and Flood Control District's Urban Storm Drainage Criteria Manual.

#### **B. Development Criteria**

There are no known constraints placed on the SITE due to floodplain studies, master studies or adjacent property drainage studies. The SITE will not receive any tributary flows from upstream land or adjacent development.

#### **C. Hydrologic Criteria**

Hydrologic calculations have been prepared in accordance with criteria set forth in the MANUAL. Refer to Appendix B for all hydrologic calculations.

#### **D. Hydraulic Criteria**

Hydraulic calculations have been prepared in accordance with criteria set forth in the MANUAL and the Urban Drainage and Flood Control District's Urban Storm Drainage Criteria Manual. Refer to Appendix C for all hydraulic calculations.

#### **E. Variance from Criteria**

No variances from criteria set forth in the MANUAL are requested at this time.

### **IV. POST-CONSTRUCTION STORMWATER MANAGEMENT**

#### **A. Stormwater Quality Control Measures**

The proposed grass lined drainage swale will provide a means for offsite run-on stormwater to be routed around the SITE during all post-construction storm events.

#### **B. Calculations**

All Hydrologic Calculations can be found in Appendix B.

All Hydraulic Calculations can be found in Appendix C.

## **V. CONCLUSIONS**

### **A. Compliance with Manual**

This report has been prepared in accordance with criteria set forth in the MANUAL and the Urban Drainage and Flood Control District's Urban Storm Drainage Criteria Manual.

### **B. Design Effectiveness**

Proper implementation of the proposed measures outlined in this report will alleviate the direct impacts of stormwater run-off on adjacent, downstream lands. The quantity of stormwater released from the SITE will be equivalent to, or less than historic conditions.

A registered licensed engineer in the state of Colorado has been consulted for the preparation of construction plans related to the recommendations outlined within this report.

### **C. Areas in Flood Hazard Zone**

The SITE is not within a FEMA-designated flood hazard zone. Refer to the FIRM Map in Appendix A for the SITE location relative to FEMA designated flood plains.

### **D. Variance from Manual**

No variances from the MANUAL are requested at this time.

## **VI. REFERENCES**

- 1) Colorado Floodplain and Stormwater Criteria Manual
- 2) Urban Drainage and Flood Control District Urban Storm Drainage and Criteria Manual, Vols. 1-3

## APPENDIX A: MAPS AND EXHIBITS



## APPENDIX B: HYDROLOGIC CALCULATIONS

DESCRIPTION  
ULTIMATE OR INITIAL  
DESIGNER  
CITY OR COUNTY

Axia Bulldog #5-31H-790 Completion Pit  
Draft Drainage Study  
MEO  
Moffat County

1 HOUR DESIGN POINT RAINFALL VALUES-NOAA ATLAS FOR COLORADO

2 YR	0.56
5 YR	0.80
10 YR	0.90
25 YR	1.10
50 YR	1.25
100 YR	1.37

24 HOUR DESIGN POINT RAINFALL VALUES-NOAA ATLAS FOR COLORADO

(MAY-OCT)

2 YR	1.10	0.95
5 YR	1.50	1.30
10 YR	1.70	1.50
25 YR	2.05	1.90
50 YR	2.25	2.10
100 YR	2.50	2.30

		Return Period					
		2-yr	5-yr	10-yr	25-yr	50-yr	100-yr
Duration	6-hr	0.86	1.15	1.30	1.55	1.70	1.90
	24-hr	1.10	1.50	1.70	2.05	2.25	2.50
	1-hr	0.56	0.80	0.90	1.10	1.25	1.37
Elevation:		6520	feet	interpolated			
		65	in hundreds of feet				

Estimating 1-hr: **Region 3:**

Yampa and Green River Basins above confluence of Green and Yampa Rivers  
From Table 11, Atlas 2, Volume 3

$$Y_2 = 0.019 + 0.711[(X_1)(X_1/X_2)] + 0.001Z$$

$$Y_{100} = 0.338 + 0.670[(X_3)(X_3/X_4)] + 0.001Z$$

$Y_2$  = 2-yr 1-hr estimated value

$Y_{100}$  = 100-yr 1-hr estimated value

$X_1$  = 2-yr 6-hr value from precipitation-frequency maps

$X_2$  = 2-yr 24-hr value from precipitation-frequency maps

$X_3$  = 100-yr 6-hr value from precipitation-frequency maps

$X_4$  = 100-yr 24-hr value from precipitation-frequency maps

Z = point elevation in hundreds of feet

**\*\*1-HR VALUES NOT VALID FOR OTHER REGIONS OF COLORADO. SEE FIGURE 19, ATLAS 2, VOL 3**

Basin	Subbasin	Undeveloped		Developed	TOTALS
Proposed		159800.5073	0	0	100000 259800.5073
	N	128893			128893.3522
	S	9506			9506
	CP	21401		100000	121401
					0
					0
					0
Existing		259800.2998	0	0	0 259800.2998
	NORTH	128893			128893.3522
	SOUTH	9506			9505.7925
	CP	121401			121401.1551

Total Site: 259800.2998

## ACRES

Basin	Subbasin	Undeveloped		Developed	TOTALS
Proposed		3.67	0.00	0.00	2.30 5.9642
	N	2.96	0.00	0.00	0.00 2.9590
		0			
	S	0.22	0.00	0.00	0.00 0.2182
		0			
	CP	0.49	0.00	0.00	2.30 2.7870
		0			
		0	0.00	0.00	0.00 0.0000
		0			
		0	0.00	0.00	0.00 0.0000
		0			
		0	0.00	0.00	0.00 0.0000
Existing		5.96	0.00	0.00	0.00 5.9642
	NORTH	2.96	0.00	0.00	0.00 2.9590
	SOUTH	0.22	0.00	0.00	0.00 0.2182
	CP	2.79	0.00	0.00	0.00 2.7870

Total Site: 5.9642

**COMPOSITE 'C' FACTORS (UNDEVELOPED)**

LOCATION: Moffat County		Draft Drainage Study										BY: MEO					Soil Type:					DATE: 7/9/2012										
BASIN DESIGNATION					UNDEVELOPED										DEVELOPED					COMPOSITE C FACTOR					% IMPERVIOUS							
	UNDEV		DEV		TOTAL	2YR	5 YR	10 YR	25 YR	100 YR	2YR	5 YR	10 YR	100 YR	2YR	5 YR	10 YR	25 YR	100 YR	2YR	5 YR	10 YR	100 YR	2YR		5 YR	10 YR	25 YR	100 YR			
	Imperviousness =					2						10																				
NORTH	2.96		0.00		2.96	0.00	0.08	0.17	0.26	0.36					0.06	0.14	0.22	0.31	0.40					0.00	0.08	0.17	0.26	0.36	2.00			
SOUTH	0.22		0.00		0.22	0.00	0.08	0.17	0.26	0.36					0.06	0.14	0.22	0.31	0.40					0.00	0.08	0.17	0.26	0.36	2.00			
CP	2.79		0.00		2.79	0.00	0.08	0.17	0.26	0.36					0.06	0.14	0.22	0.31	0.40					0.00	0.08	0.17	0.26	0.36	2.00			
																							COMPOSITE I, %					TOTAL A, ac				
																							2.00					3.18				



Axia Energy Completion Pit  
Bulldog #5-31H-790

**STORM DRAINAGE SYSTEM DESIGN**  
**(RATIONAL METHOD PROCEDURE, STANDARD FOR SF-3)**  
**DESIGN STORM: 25-YEAR UNDEVELOPED**

Calc. by: MEO  
Chk'd by: WEP  
Date: 7/9/2012

Axia Bulldog #5-31H-790 Completion Pit

Draft Drainage Study

Moffat County

DESIGN POINT	DIRECT RUNOFF							TOTAL RUNOFF					DITCH		TRAVEL TIME			REMARKS
	BASIN	AREA (AC)	COEFF. (C)	Tc (Min.)	C*A	I (in./hr.)	Q (cfs)	Sum Area	Tc (min)	I (in./hr.)	Sum C*A	Total Q (cfs)	SLOPE %	FLOW (CFS)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME Tt	
	NORTH	2.96	0.26	14.98	0.77	2.53	1.94											North Swale at culvert under Access Road
	SOUTH	0.22	0.26	12.13	0.06	2.79	0.16											South Swale
	CP	2.79	0.26	9.49	0.72	3.08	2.22											Completion Pit area

**STORM DRAINAGE SYSTEM DESIGN**  
**(RATIONAL METHOD PROCEDURE, STANDARD FOR SF-3)**  
**DESIGN STORM: 100-YEAR UNDEVELOPED**

Calc. by: MEO  
 Chk'd by: WEP  
 Date: 7/9/2012

Axia Bulldog #5-31H-790 Completion Pit

Draft Drainage Study

Moffat County

DESIGN POINT	DIRECT RUNOFF							TOTAL RUNOFF					DITCH		TRAVEL TIME			REMARKS
	BASIN	AREA (AC)	COEFF. (C)	Tc (Min.)	C*A	I (in./hr.)	Q (cfs)	Sum Area	Tc (min)	I (in./hr.)	Sum C*A	Total Q (cfs)	SLOPE %	FLOW (CFS)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME Tt	
	NORTH	2.96	0.36	14.98	1.07	3.16	3.38											North Swale at culvert under Access Road
	SOUTH	0.22	0.36	12.13	0.08	3.47	0.27											South Swale
	CP	2.79	0.36	9.49	1.01	3.84	3.87											Completion Pit area

DESCRIPTION  
ULTIMATE OR INITIAL  
DESIGNER  
CITY OR COUNTY

Axia Bulldog #5-31H-790 Completion Pit Draft Drainage Study MEO Moffat County
--

1 HOUR DESIGN POINT RAINFALL VALUES-NOAA ATLAS FOR COLORADO

2 YR	0.56
5 YR	0.80
10 YR	0.90
25 YR	1.10
50 YR	1.25
100 YR	1.37

24 HOUR DESIGN POINT RAINFALL VALUES-NOAA ATLAS FOR COLORADO

(MAY-OCT)

2 YR	1.10	0.95
5 YR	1.50	1.30
10 YR	1.70	1.50
25 YR	2.05	1.90
50 YR	2.25	2.10
100 YR	2.50	2.30

		Return Period					
		2-yr	5-yr	10-yr	25-yr	50-yr	100-yr
Duration	6-hr	0.86	1.15	1.30	1.55	1.70	1.90
	24-hr	1.10	1.50	1.70	2.05	2.25	2.50
	1-hr	0.56	0.80	0.90	1.10	1.25	1.37
Elevation:		6520	feet	interpolated			
		65	in hundreds of feet				

Estimating 1-hr: **Region 3:**

Yampa and Green River Basins above confluence of Green and Yampa Rivers  
From Table 11, Atlas 2, Volume 3

$$Y_2 = 0.019 + 0.711[(X_1)(X_1/X_2)] + 0.001Z$$

$$Y_{100} = 0.338 + 0.670[(X_3)(X_3/X_4)] + 0.001Z$$

$Y_2$  = 2-yr 1-hr estimated value

$Y_{100}$  = 100-yr 1-hr estimated value

$X_1$  = 2-yr 6-hr value from precipitation-frequency maps

$X_2$  = 2-yr 24-hr value from precipitation-frequency maps

$X_3$  = 100-yr 6-hr value from precipitation-frequency maps

$X_4$  = 100-yr 24-hr value from precipitation-frequency maps

Z = point elevation in hundreds of feet

**\*\*1-HR VALUES NOT VALID FOR OTHER REGIONS OF COLORADO. SEE FIGURE 19, ATLAS 2, VOL 3**

Basin	Subbasin	Undeveloped		Developed	TOTALS
Proposed		158746.4	0	0	100000 258746.4
	N	127631			127630.8
	S	8276			8276.4
	CP	22839		100000	122839
					0
					0
					0
Existing		259800.2998	0	0	0 259800.2998
	NORTH	128893			128893.3522
	SOUTH	9506			9505.7925
	CP	121401			121401.1551

Total Site: 258746.4

## ACRES

Basin	Subbasin	Undeveloped		Developed	TOTALS
Proposed		3.64	0.00	0.00	2.30 5.9400
	N	2.93	0.00	0.00	0.00 2.9300
		0			
	S	0.19	0.00	0.00	0.00 0.1900
		0			
	CP	0.52	0.00	0.00	2.30 2.8200
		0			
		0	0.00	0.00	0.00 0.0000
		0			
		0	0.00	0.00	0.00 0.0000
		0			
		0	0.00	0.00	0.00 0.0000
Existing		5.96	0.00	0.00	0.00 5.9642
	NORTH	2.96	0.00	0.00	0.00 2.9590
	SOUTH	0.22	0.00	0.00	0.00 0.2182
	CP	2.79	0.00	0.00	0.00 2.7870

Total Site: 5.9400

**COMPOSITE 'C' FACTORS (DEVELOPED)**

LOCATION: Moffat County		Draft Drainage Study										BY: MEO					Soil Type: B				DATE: 7/9/2012								
BASIN DESIGNATION					UNDEVELOPED										DEVELOPED					COMPOSITE C FACTOR					% IMPERVIOUS				
	UNDEV		DEV		TOTAL	2YR	5 YR	10 YR	25 YR	100 YR	2YR	5 YR	10 YR	100 YR	2YR	5 YR	10 YR	25 YR	100 YR	2YR	5 YR	10 YR	100 YR	2YR		5 YR	10 YR	25 YR	100 YR
	Imperviousness =					2						100																	
NORTH	2.93		0.00		2.93	0.00	0.08	0.17	0.26	0.36					0.89	0.90	0.92	0.94	0.96					0.00	0.08	0.17	0.26	0.36	2.00
SOUTH	0.19		0.00		0.19	0.00	0.08	0.17	0.26	0.36					0.89	0.90	0.92	0.94	0.96					0.00	0.08	0.17	0.26	0.36	2.00
CP	0.52		2.30		2.82	0.00	0.08	0.17	0.26	0.36					0.89	0.90	0.92	0.94	0.96					0.72	0.74	0.78	0.81	0.85	81.78
																								COMPOSITE I, %					TOTAL A, ac
																								39.87					5.94



Axia Energy Completion Pit  
Bulldog #5-31H-790

**STORM DRAINAGE SYSTEM DESIGN**  
**(RATIONAL METHOD PROCEDURE, STANDARD FOR SF-3)**  
**DESIGN STORM: 25-YEAR DEVELOPED**

Calc. by: MEO  
Chk'd by: WEP  
Date: 7/9/2012

Axia Bulldog #5-31H-790 Completion Pit

Draft Drainage Study

Moffat County

DESIGN POINT	DIRECT RUNOFF							TOTAL RUNOFF					DITCH		TRAVEL TIME			REMARKS
	BASIN	AREA (AC)	COEFF. (C)	Tc (Min.)	C*A	I (in./hr.)	Q (cfs)	Sum Area	Tc (min)	I (in./hr.)	Sum C*A	Total Q (cfs)	SLOPE %	FLOW (CFS)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME Tt	
	NORTH	2.93	0.26	14.99	0.76	2.53	1.92											North Swale at culvert under Access Road
	SOUTH	0.19	0.26	12.13	0.05	2.79	0.14											South Swale
	CP	2.82	0.81	6.77	2.28	3.47	7.92											Completion Pit area

**STORM DRAINAGE SYSTEM DESIGN**  
**(RATIONAL METHOD PROCEDURE, STANDARD FOR SF-3)**  
**DESIGN STORM: 100-YEAR DEVELOPED**

Calc. by: MEO  
 Chk'd by: WEP  
 Date: 7/9/2012

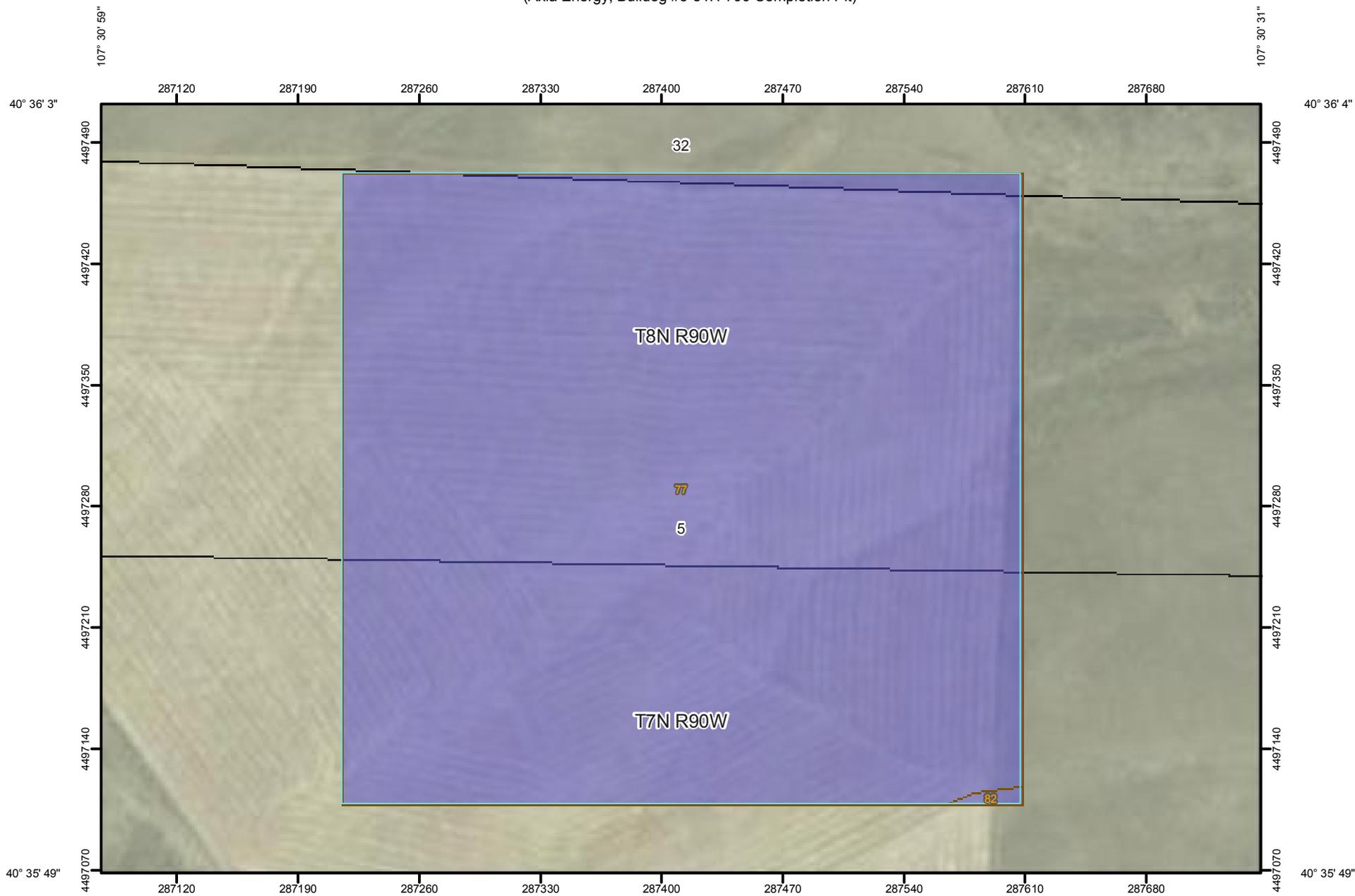
Axia Bulldog #5-31H-790 Completion Pit

Draft Drainage Study

Moffat County

DESIGN POINT	DIRECT RUNOFF							TOTAL RUNOFF					DITCH		TRAVEL TIME			REMARKS
	BASIN	AREA (AC)	COEFF. (C)	Tc (Min.)	C*A	I (in./hr.)	Q (cfs)	Sum Area	Tc (min)	I (in./hr.)	Sum C*A	Total Q (cfs)	SLOPE %	FLOW (CFS)	LENGTH (FT)	VEL. (FPS)	TRAVEL TIME Tt	
	NORTH	2.93	0.36	14.99	1.06	3.16	3.35											North Swale at culvert under Access Road
	SOUTH	0.19	0.36	12.13	0.07	3.47	0.24											South Swale
	CP	2.82	0.85	6.77	2.38	4.32	10.30											Completion Pit area

Hydrologic Soil Group—Moffat County Area, Colorado  
(Axia Energy, Bulldog #5-31H-790 Completion Pit)



Map Scale: 1:3,180 if printed on A size (8.5" x 11") sheet.



## MAP LEGEND

### Area of Interest (AOI)

 Area of Interest (AOI)

### Soils

 Soil Map Units

### Soil Ratings

 A  
 A/D  
 B  
 B/D  
 C  
 C/D  
 D  
 Not rated or not available

### Political Features

 Cities  
 PLSS Township and Range  
 PLSS Section

### Water Features

 Streams and Canals

### Transportation

 Rails  
 Interstate Highways  
 US Routes  
 Major Roads  
 Local Roads

## MAP INFORMATION

Map Scale: 1:3,180 if printed on A size (8.5" × 11") sheet.

The soil surveys that comprise your AOI were mapped at 1:31,680.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for accurate map measurements.

Source of Map: Natural Resources Conservation Service  
Web Soil Survey URL: <http://websoilsurvey.nrcs.usda.gov>  
Coordinate System: UTM Zone 13N NAD83

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Moffat County Area, Colorado  
Survey Area Data: Version 6, Feb 4, 2008

Date(s) aerial images were photographed: 8/28/2005

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Hydrologic Soil Group

Hydrologic Soil Group— Summary by Map Unit — Moffat County Area, Colorado (CO686)				
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
77	Forelle loam, 3 to 12 percent slopes	B	35.2	99.8%
82	Forelle-Pinelli-Maysprings complex, 5 to 20 percent slopes	B	0.1	0.2%
<b>Totals for Area of Interest</b>			<b>35.2</b>	<b>100.0%</b>

### Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

### Rating Options

*Aggregation Method:* Dominant Condition

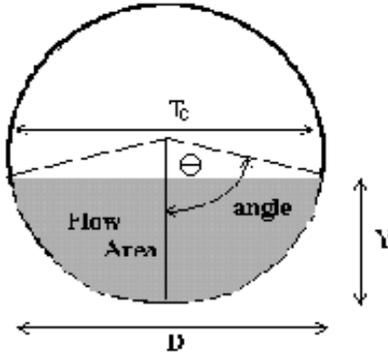
*Component Percent Cutoff:* None Specified

*Tie-break Rule:* Higher

## APPENDIX C: HYDRAULIC CALCULATIONS

## CIRCULAR CONDUIT FLOW (Normal & Critical Depth Computation)

Project: **Axia Energy Completion Pit**  
 Pipe ID: **Access Road Swale Crossing**



### Design Information (Input)

Pipe Invert Slope	So =	0.0590	ft/ft
Pipe Manning's n-value	n =	0.0240	*
Pipe Diameter	D =	12.00	inches
<b>Design discharge</b>	<b>Q =</b>	<b>4.70</b>	<b>cfs</b>

### Full-flow Capacity (Calculated)

Full-flow area	Af =	0.79	sq ft
Full-flow wetted perimeter	Pf =	3.14	ft
Half Central Angle	Theta =	3.14	radians
Full-flow capacity	Qf =	4.70	cfs

### Calculation of Normal Flow Condition

Half Central Angle ( $0 < \theta < 3.14$ )	Theta =	2.26	radians
Flow area	An =	0.69	sq ft
Top width	Tn =	0.77	ft
Wetted perimeter	Pn =	2.26	ft
Flow depth	Yn =	0.82	ft
Flow velocity	Vn =	6.82	fps
Discharge	Qn =	4.70	cfs
Percent Full Flow	Flow =	100.00%	of full flow
Normal Depth Froude Number	Fr <sub>n</sub> =	1.27	supercritical

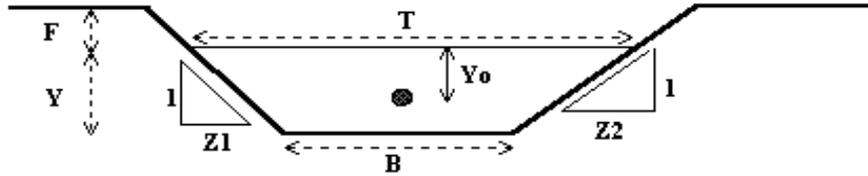
### Calculation of Critical Flow Condition

Half Central Angle ( $0 < \theta_c < 3.14$ )	Theta-c =	2.50	radians
Critical flow area	Ac =	0.74	sq ft
Critical top width	Tc =	0.60	ft
Critical flow depth	Yc =	0.90	ft
Critical flow velocity	Vc =	6.31	fps
Critical Depth Froude Number	Fr <sub>c</sub> =	1.00	

\* Unexpected value for Manning's n

## Normal Flow Analysis - Trapezoidal Channel

Project: **Axia Bulldog #5-31H-790 Completion Pit**  
 Channel ID: **Swales**



<b>Design Information (Input)</b>	
Channel Invert Slope	So = <u>0.0300</u> ft/ft
Manning's n	n = <u>0.030</u>
Bottom Width	B = <u>0.00</u> ft
Left Side Slope	Z1 = <u>3.00</u> ft/ft
Right Side Slope	Z2 = <u>3.00</u> ft/ft
Freeboard Height	F = <u>0.00</u> ft
Design Water Depth	Y = <u>1.00</u> ft
<b>Normal Flow Condition (Calculated)</b>	
<b>Discharge</b>	<b>Q = <u>15.70</u> cfs</b>
<b>Froude Number</b>	<b>Fr = <u>1.30</u></b>
<b>Flow Velocity</b>	<b>V = <u>5.23</u> fps</b>
Flow Area	A = <u>3.00</u> sq ft
Top Width	T = <u>6.00</u> ft
Wetted Perimeter	P = <u>6.32</u> ft
Hydraulic Radius	R = <u>0.47</u> ft
Hydraulic Depth	D = <u>0.50</u> ft
Specific Energy	Es = <u>1.43</u> ft
Centroid of Flow Area	Yo = <u>0.33</u> ft
Specific Force	Fs = <u>0.22</u> kip